L Number	Hits	Search Text	DB	Time stamp
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3	5	finite adj element adj analysis adj mesh and (weld\$. –	2002/12/21
–	5	stress\$ distort\$) and (@ad<19991127 @rlad<19991127)	USPAT;	2003/12/31
		Siressa distorta) and (@ddx13331127 @riddx13331127)	US-PGPUB;	10:36
			EPO; JPO;	
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5	96	finite adj element adj analysis and weld\$ and stress\$	USPAT;	2003/12/31
		and distort\$ and (@ad<19991127 @rlad<19991127)	US-PGPUB;	10:34
ļ			EPO; JPO;	
			DERWENT;	
	_		IBM_TDB	
6	0	finite adj element adj analysis and analytical adj solution	USPAT:	2003/12/31
		and weld\$ and stress\$ and distort\$ and (@ad<19991127	US-PGPUB;	10:36
		@rlad<19991127)	EPO; JPO;	
			DERWENT;	
ļ			IBW_TDB	
7	693	analytical adj solution and (@ad<19991127	USPAT;	2003/12/31
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			EPO; JPO;	
			DERWENT;	
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8	. 43	analytical adj solution and weld\$ and (@ad<19991127	USPAT;	2003/12/31
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			DERWENT;	1
İ			IBM_TDB	
9	259	analytical adj solution and (weld\$ stress\$ distort\$) and	USPAT;	2003/12/31
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		(EPO; JPO;	13.55
			DERWENT;	
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10	9	finite adj element adj analysis and analytical adj solution	USPAT;	2003/12/31
_		and (weld\$ stress\$ distort\$) and (@ad<19991127	US-PGPUB;	10:37
		@rlad<19991127)	EPO; JPO;	10.37
			DERWENT;	
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11	2	finite adi alement adi analysis and analytical adi advetu	IBM_TDB	2002/12/24
	۲	finite adj element adj analysis and analytical adj solution	USPAT;	2003/12/31
	ļ	and weld\$ and (stress\$ distort\$) and (@ad<19991127	US-PGPUB;	10:39
		@rlad<19991127)	EPO; JPO;	
			DERWENT;	
			IBM_TDB	

13	1157	model and weld\$ and stress\$ and distort\$ and	USPAT;	2003/12/31
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		(3.00 577755 3.100 57775)	EPO; JPO;	
			DERWENT;	
		·	IBM_TDB	
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. - '		(@ad<19991127 @rlad<19991127)	US-PGPUB;	10:40
		(666-1555-1-17)	EPO; JPO;	
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		,	EPO; JPO;	
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		solution) and weld\$ and stress\$ and distort\$ and	US-PGPUB;	10:43
		(@ad<19991127 @rlad<19991127)	EPO; JPO;	•
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17	9	model and mesh and (finite element) and (analytical	USPAT;	2003/12/31
		solution) and weld\$ and residual adj stress\$ and	US-PGPUB;	10:44
		(distort\$ deform\$) and (@ad<19991127	EPO; JPO;	
		@rlad<19991127)	DERWENT;	
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		solution) and weld\$ and residual adj stress\$ and	US-PGPUB;	10:54
		(distort\$ deform\$) and structur\$ and (@ad<19991127	EPO; JPO;	
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		@rlad<19991127)	US-PGPUB;	
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			DERWENT;	
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		element) stress) and (@ad<19991127 @rlad<19991127)	US-PGPUB;	
			EPO; JPO;	
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22		702/4 111 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	IBM_TDB	
22	2	703/\$ and thermal near analysis same ((analytical near	USPAT;	2003/12/31 11:12
		solution) (deform\$ distort\$)) and (@ad<19991127	US-PGPUB;	
		@rlad<19991127)	EPO; JPO;	
			DERWENT;	
22		F70//17	IBM_TDB	2002 (12 (2: :: :=
23	2	5796617.pn.	USPAT;	2003/12/31 11:35
			US-PGPUB;	
			EPO; JPO;	
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24	0	703/\$ and weld\$ and thermal near analysis same (((finite	USPAT;	2003/12/31 11:56
		near element) and stress) ((analytical near solution) and	US-PGPUB;	
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	1	@rlad<19991127)	DERWENT;	
			IBW_TDB	
25	0	703/\$ and weld\$ and thermal near analysis and (((finite	USPAT;	2003/12/31 11:56
		near element) and stress) ((analytical near solution) and	US-PGPUB;	
		(deform\$ distort\$))) and (@ad<19991127	EPO; JPO;	
		@rlad<19991127)	DERWENT;	
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		near element) and stress) ((analytical near solution) and	US-PGPUB;	
:		(deform\$ distort\$))) and (@ad<19991127	EPO; JPO;	
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27	o	700/\$ and weld\$ and thermal near analysis same (((finite	USPAT;	2003/12/31 11:57
		near element) and stress) ((analytical near solution) and	US-PGPUB;	
		(deform\$ distort\$))) and (@ad<19991127	EPO; JPO;	
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	1.		IBM_TDB	
28	2	weld\$ and thermal near analysis same (((finite near	USPAT;	2003/12/31
	_	element) and stress) ((analytical near solution) and	US-PGPUB;	12:02
		(deform\$ distort\$))) and (@ad<19991127	EPO; JPO;	12.02
	1	@rlad<19991127)	DERWENT;	:
			IBM_TDB	
29	19	weld\$ and thermal near analysis and (((finite near	USPAT;	2003/12/31 12:11
-		element) and stress) ((analytical near solution) and	US-PGPUB;	2000/12/01 12:11
		(deform\$ distort\$))) and (@ad<19991127	EPO; JPO;	
<u> </u>		@rlad<19991127)	DERWENT;	
	İ	C (100 - 122)	IBM_TDB	
30	o	weld\$ and thermal near analysis and (finite near element)	USPAT;	2003/12/31 12:12
		and stress and (analytical near solution) and (deform\$	US-PGPUB;	2000,12,011212
		distort\$) and (@ad<19991127 @rlad<19991127)	EPO; JPO;	
			DERWENT;	
			IBM_TDB	
31	12	weld\$ and thermal near analysis and (finite near element)	USPAT;	2003/12/31 12:15
		and stress and (deform\$ distort\$) and (@ad<19991127	US-PGPUB;	
		@rlad<19991127)	EPO; JPO;	
		,	DERWENT;	
			IBM_TDB	
32	6	weld\$ and thermal near analysis and (finite near element)	USPAT;	2003/12/31 12:18
		and analysis same (stress and (deform\$ distort\$)) and	US-PGPUB;	
		(@ad<19991127 @rlad<19991127)	EPO; JPO;	
		(DERWENT;	
			IBM_TDB	
33	19	weld\$ and thermal near analysis and analysis same	USPAT;	2003/12/31 12:21
	1	(deform\$ distort\$) and (@ad<19991127	US-PGPUB;	
		@rlad<19991127)	EPO; JPO;	
]		DERWENT;	
			IBM_TDB	
34	16	weld\$ and thermal near analysis and analysis same	USPAT;	2003/12/31
		(stress and deform\$ distort\$) and (@ad<19991127	US-PGPUB;	12:23
		@rlad<19991127)	EPO; JPO;	
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35		molde and the arms and analysis same	LICDAT	2002/12/21
39	8	weld\$ and thermal near analysis and analysis same	USPAT;	2003/12/31
		(stress and (deform\$ distort\$)) and (@ad<19991127	US-PGPUB;	12:25
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]	and (@ad<19991127 @rlad<19991127)	US-PGPUB;	12:25
			EPO; JPO;	
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37	4	(703/2 703/6 703/7) and weld\$ and analysis same	USPAT;	2003/12/31
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38	1	700/98 and weld\$ and analysis same (stress and	USPAT;	2003/12/31 12:31
	,	(deform\$ distort\$)) and (@ad<19991127	US-PGPUB;	
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			DERWENT;	
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39	1	700/98 and weld\$ and analysis and (stress and (deform\$	USPAT;	2003/12/31 12:31
	1	distort\$)) and (@ad<19991127 @rlad<19991127)	US-PGPUB;	2003/12/31 12:31
		distor (\$)) and (@dd(19991127 @Hdd(19991127)	1	
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40		(702/2702/7702/77)	IBM_TDB	0000 (10 (0)
40	6	(703/2 703/6 703/7) and weld\$ and analysis and (stress	USPAT;	2003/12/31
		and (deform\$ distort\$)) and (@ad<19991127	US-PGPUB;	12:32
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			DERWENT;	
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44	2	09/270007	USPAT;	2003/12/31 13:11
		•	US-PGPUB;	
			EPO; JPO;	
			DERWENT;	
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45	3	"09311150"	USPAT;	2003/12/31 13:11
			US-PGPUB;	
			EPO; JPO;	
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46	2	adiabatic near boundary and (@ad<19991127	USPAT;	2003/12/31 15:17
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			EPO; JPO;	
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			IBM_TDB	
47	15449	adiabatic and (@ad<19991127 @rlad<19991127)	USPAT;	2003/12/31 15:15
			US-PGPUB;	
			EPO; JPO;	
			DERWENT;	
			IBM_TDB	
48	17	703/\$ and adiabatic and (@ad<19991127	USPAT;	2003/12/31 15:15
· -	''	@rlad<19991127)	US-PGPUB;	
		C. 1997777777)	EPO; JPO;	
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49	1	703/\$ and adiabatic with boundary and (@ad<19991127	USPAT;	2003/12/31 15:18
		@rlad<19991127)	US-PGPUB;	
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50	59	703/\$ and conduct\$ with boundary and (@ad<19991127	USPAT;	2003/12/31 15:19
		@rlad<19991127)	US-PGPUB;	
			EPO; JPO;	
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51	6	703/\$ and conduct\$ near boundary and (@ad<19991127	USPAT;	2003/12/31
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			EPO; JPO;	
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	_	<u>.</u>	IBW_TDB	
52	6	reflected near heat near source and (@ad<19991127	USPAT;	2003/12/31 15:21
		@rlad<19991127)	US-PGPUB;	
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53	389	boundary same heat near source and (@ad<19991127	USPAT;	2003/12/31 15:21
		@rlad<19991127)	US-PGPUB;	
			EPO; JPO;	
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54	5	boundary same (reflected point) near heat near source	USPAT;	2003/12/31
		and (@ad<19991127 @rlad<19991127)	US-PGPUB;	15:22
			EPO; JPO;	
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83	. 2	6324491.pn.	USPAT;	2003/12/31
			US-PGPUB;	18:00
			EPO; JPO;	
			DERWENT;	
		703/3 1 (1-14 1-144 1	IBM_TDB	2002/12/21
-	9	703/2 and (model\$ simulat\$) same weld\$ and	USPAT;	2003/12/31
		(@ad<19991127 @rlad<19991127)	US-PGPUB;	10:30
			EPO; JPO;	
	i		DERWENT; IBM_TDB	
_	12	703/2 and (model\$ simulat\$) and weld\$ and (stress	USPAT;	2003/12/30
_	12	distort\$) and (@ad<19991127 @rlad<19991127)	US-PGPUB;	17:25
		distorty) and (@ddx133391127 @Mddx133391127)	EPO; JPO;	17.25
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_	96	703/2 and (model\$ simulat\$) and (coordinat\$ node	USPAT;	2003/12/30
	. 70	mesh) and (stress distort\$) and (@ad<19991127	US-PGPUB;	17:26
		@rlad<19991127)	EPO; JPO;	17.20
		C. 100-12/2110/	DERWENT;	
			IBM_TDB	
_	34	703/2 and (model\$ simulat\$) and (coordinat\$ node	USPAT;	2003/12/30
	77	mesh) and (stress distort\$) and (weld\$ thermal) and	US-PGPUB;	17:33
		(@ad<19991127 @rlad<19991127)	EPO; JPO;	17.55
		(Guarissite)	DERWENT;	
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-	2	6398102.pn.	USPAT;	2003/12/30
		·	US-PGPUB;	17:32
			EPO; JPO;	
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			IBM_TDB	
-	45	703/2 and (model\$ simulat\$) and (coordinat\$ node	USPAT;	2003/12/30
		mesh) and (stress distort\$) and (weld\$ thermal	US-PGPUB;	17:34
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-	30	703/2 and (model\$ simulat\$) same (stress distort\$) and	USPAT;	2003/12/30
		(coordinat\$ node mesh) and (weld\$ thermal	US-PGPUB;	19:52
		temperature) and (@ad<19991127 @rlad<19991127)	EPO; JPO;	
			DERWENT;	
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-	7	703/2 and (model\$ simulat\$) same (stress distort\$)	USPAT;	2003/12/30
		same (coordinat\$ node mesh) same (weld\$ thermal	US-PGPUB;	19:52
		temperature) and (@ad<19991127 @rlad<19991127)	EPO; JPO;	
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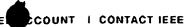
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[Abstract]

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[Abstract]



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	3 A hybrid resonant converter operated as a low had and without active control Belaguli, V.; Bhat, A.K.S.; Power Electronics Specialists Conference, 1996. PESC '96 IEEE, Volume: 1', 23-27 June 1996					

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